## FEATURES

True single-supply operation

Output swings rail-to-rail

Input voltage range extends below ground

Single-supply capability from 3 V to 36 V

Dual-supply capability from $\pm 1.5 \mathrm{~V}$ to $\pm 18 \mathrm{~V}$

High load drive
Capacitive load drive of $\mathbf{3 5 0} \mathbf{~ p F , G}=+1$
Minimum output current of 15 mA
Excellent ac performance for low power
$800 \mu \mathrm{~A}$ maximum quiescent current per amplifier
Unity gain bandwidth: 1.8 MHz
Slew rate of $3.0 \mathrm{~V} / \mathrm{ms}$
Good dc performance
$800 \mu \mathrm{~V}$ maximum input offset voltage
$2 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ typical offset voltage drift
25 pA maximum input bias current
Low noise
13 nV/VHz @ 10 kHz
No phase inversion

## APPLICATIONS

## Battery-powered precision instrumentation

Photodiode preamps
Active filters
12-bit to 14-bit data acquisition systems
Medical instrumentation
Low power references and regulators

## FUNCTIONAL BLOCK DIAGRAM



Figure 1. 8-Lead PDIP (N Suffix); 8-Lead MSOP (RM Suffix); and 8-Lead SOIC (R Suffix)

## GENERAL DESCRIPTION

The AD822 is a dual precision, low power FET input op amp that can operate from a single supply of 3.0 V to 36 V or dual supplies of $\pm 1.5 \mathrm{~V}$ to $\pm 18 \mathrm{~V}$. It has true single-supply capability with an input voltage range extending below the negative rail, allowing the AD822 to accommodate input signals below ground in the single-supply mode. Output voltage swing extends to within 10 mV of each rail, providing the maximum output dynamic range.


Figure 2. Input Voltage Noise vs. Frequency
Offset voltage of $800 \mu \mathrm{~V}$ maximum, offset voltage drift of $2 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$, input bias currents below 25 pA , and low input voltage noise provide dc precision with source impedances up to a $\mathrm{G} \Omega .1 .8 \mathrm{MHz}$ unity gain bandwidth, -93 dB THD at 10 kHz , and $3 \mathrm{~V} / \mu \mathrm{s}$ slew rate are provided with a low supply current of $800 \mu \mathrm{~A}$ per amplifier.
(continued on Page 3)

Rev, F
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## TABLE OF CONTENTS

Features ..... 1
Applications. ..... 1
Functional Block Diagram .....  1
General Description ..... 1
Revision History ..... 2
Specifications ..... 4
Absolute Maximum Ratings ..... 10
Maximum Power Dissipation ..... 10
ESD Caution ..... 10
Typical Performance Characteristics ..... 11
Application Notes ..... 18
REVISION HISTORY
10/05-Rev. E to Rev. F
Updated Format ..... Universal
Changes to Outline Dimensions ..... 24
Updated Ordering Guide ..... 24
1/03-Data sheet changed from Rev. D to Rev. E Edits to Specifications ..... 2
Edits to Figure 10 ..... 16
Updated Outline Dimensions ..... 17
10/02-Data sheet changed from Rev. C to Rev. D
Edits to Features ..... 1
Edits to Ordering Guide ..... 6
Updated SOIC Package Outline ..... 17
Input Characteristics ..... 18
Output Characteristics ..... 18
Applications ..... 20
Single-Supply Voltage-to-Frequency Converter ..... 20
Single-Supply Programmable Gain Instrumentation Amplifier ..... 20
3 V, Single-Supply Stereo Headphone Driver ..... 21
Low Dropout Bipolar Bridge Driver ..... 21
Outline Dimensions ..... 22
Ordering Guide ..... 23
8/02-Data sheet changed from Rev. B to Rev. C
All Figures Updated ..... Global
Edits to Features. .....  1
Updated All Package Outlines ..... 17
7/01-Data sheet changed from Rev. A to Rev. B
All Figures Updated ..... Global
CERDIP References Removed ..... 1,6 , and 18
Additions to Product Description .....  1
8-Lead SOIC and 8-Lead MSOP Diagrams Added .....  1
Deletion of AD822S Column ..... 2
Edits to Absolute Maximum Ratings and Ordering Guide ..... 6
Removed Metalization Photograph ..... 6

## GENERAL DESCRIPTION

## (continued from Page 1)

The AD822 drives up to 350 pF of direct capacitive load as a follower and provides a minimum output current of 15 mA . This allows the amplifier to handle a wide range of load conditions. Its combination of ac and dc performance, plus the outstanding load drive capability, results in an exceptionally versatile amplifier for the single-supply user.

The AD822 is available in two performance grades. The A grade and $B$ grade are rated over the industrial temperature range of $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$.

The AD822 is offered in three varieties of 8-lead packages: PDIP, MSOP, and SOIC.


Figure 3. Gain-of-2 Amplifier; $V_{S}=5,0, V_{I N}=2.5 \mathrm{~V}$ Sine Centered at 1.25 V, $R L=100 \Omega$

## AD822

## SPECIFICATIONS

$\mathrm{V}_{\mathrm{S}}=0,5 \mathrm{~V} @ \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{CM}}=0 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}=0.2 \mathrm{~V}$, unless otherwise noted.
Table 1.

| Parameter | Condition | AD822 A Grade |  |  | AD822 B Grade |  |  | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Min | Typ | Max | Min | Typ | Max |  |
| DC PERFORMANCE |  |  |  |  |  |  |  |  |
| Initial Offset |  |  | 0.1 | 0.8 |  | 0.1 | 0.4 | mV |
| Maximum Offset Overtemperature |  |  | 0.5 | 1.2 |  | 0.5 | 0.9 | mV |
| Offset Drift |  |  | 2 |  |  | 2 |  | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
| Input Bias Current | $\mathrm{V}_{\text {СM }}=0 \mathrm{~V}$ to 4 V |  | 2 | 25 |  | 2 | 10 | pA |
| at Tmax |  |  | 0.5 | 5 |  | 0.5 | 2.5 | nA |
| Input Offset Current |  |  | 2 | 20 |  | 2 | 10 | pA |
| at $\mathrm{T}_{\text {max }}$ |  |  | 0.5 |  |  | 0.5 |  | nA |
| Open-Loop Gain | $\mathrm{V}_{\mathrm{O}}=0.2 \mathrm{~V}$ to 4 V |  |  |  |  |  |  |  |
|  | $\mathrm{RL}=100 \mathrm{k} \Omega$ | 500 | 1000 |  | 500 | 1000 |  | $\mathrm{V} / \mathrm{mV}$ |
| $\mathrm{T}_{\text {MIN }}$ to $\mathrm{T}_{\text {MAX }}$ |  | 400 |  |  | 400 |  |  | $\mathrm{V} / \mathrm{mV}$ |
|  | $\mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega$ | 80 | 150 |  | 80 | 150 |  | $\mathrm{V} / \mathrm{mV}$ |
| $\mathrm{T}_{\text {min }}$ to $\mathrm{T}_{\text {max }}$ |  | 80 |  |  | 80 |  |  | $\mathrm{V} / \mathrm{mV}$ |
|  | $\mathrm{R}_{\mathrm{L}}=1 \mathrm{k} \Omega$ | 15 | 30 |  | 15 | 30 |  | $\mathrm{V} / \mathrm{mV}$ |
| $\mathrm{T}_{\text {MIN }}$ to $\mathrm{T}_{\text {MAX }}$ |  | 10 |  |  | 10 |  |  | $\mathrm{V} / \mathrm{mV}$ |
| NOISE/HARMONIC PERFORMANCE Input Voltage Noise |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |
| 0.1 Hz to 10 Hz |  |  | 2 |  |  | 2 |  | $\mu \mathrm{V}$ p-p |
| $\mathrm{f}=10 \mathrm{~Hz}$ |  |  | 25 |  |  | 25 |  | $\mathrm{nV} / \sqrt{ } \mathrm{Hz}$ |
| $\mathrm{f}=100 \mathrm{~Hz}$ |  |  | 21 |  |  | 21 |  | $\mathrm{nV} / \sqrt{ } \mathrm{Hz}$ |
| $\mathrm{f}=1 \mathrm{kHz}$ |  |  | 16 |  |  | 16 |  | $\mathrm{nV} / \sqrt{ } \mathrm{Hz}$ |
| $\mathrm{f}=10 \mathrm{kHz}$ |  |  | 13 |  |  | 13 |  | $\mathrm{nV} / \sqrt{ } \mathrm{Hz}$ |
| Input Current Noise |  |  |  |  |  |  |  |  |
| 0.1 Hz to 10 Hz |  |  | 18 |  |  | 18 |  | fA p-p |
| $\mathrm{f}=1 \mathrm{kHz}$ |  |  | 0.8 |  |  | 0.8 |  | $\mathrm{fA} / \sqrt{ } \mathrm{Hz}$ |
| Harmonic Distortion | $\mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega$ to 2.5 V |  |  |  |  |  |  |  |
| $\mathrm{f}=10 \mathrm{kHz}$ | $\mathrm{V}_{\mathrm{o}}=0.25 \mathrm{~V}$ to 4.75 V |  | -93 |  |  | -93 |  | dB |
| DYNAMIC PERFORMANCE |  |  |  |  |  |  |  |  |
| Unity Gain Frequency |  |  | 1.8 |  |  | 1.8 |  | MHz |
| Full Power Response | $\mathrm{V}_{\circ} \mathrm{p}-\mathrm{p}=4.5 \mathrm{~V}$ |  | 210 |  |  | 210 |  | kHz |
| Slew Rate |  |  | 3 |  |  | 3 |  | $\mathrm{V} / \mathrm{\mu s}$ |
| Settling Time |  |  |  |  |  |  |  |  |
| to 0.1\% | $\mathrm{V}_{\mathrm{o}}=0.2 \mathrm{~V}$ to 4.5 V |  | 1.4 |  |  | 1.4 |  | $\mu \mathrm{s}$ |
| to 0.01\% |  |  | 1.8 |  |  | 1.8 |  | $\mu \mathrm{s}$ |
| MATCHING CHARACTERISTICS |  |  |  |  |  |  |  |  |
| Initial Offset |  |  |  | 1.0 |  |  | 0.5 | mV |
| Maximum Offset overtemperature |  |  |  | 1.6 |  |  | 1.3 | mV |
| Offset Drift |  |  | 3 |  |  | 3 |  | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
| Input Bias Current |  |  |  | 20 |  |  | 10 |  |
| Crosstalk @ $\mathrm{f}=1 \mathrm{kHz}$ | $\mathrm{RL}=5 \mathrm{k} \Omega$ |  | -130 |  |  | -130 |  | dB |
| $\mathrm{f}=100 \mathrm{kHz}$ |  |  |  |  |  |  |  |  |
| INPUT CHARACTERISTICS |  |  |  |  |  |  |  |  |
| Input Voltage Range ${ }^{1}$ |  | -0.2 |  | +4 | -0.2 |  | +4 | V |
| $\mathrm{T}_{\text {min }}$ to $\mathrm{T}_{\text {max }}$ |  | -0.2 |  | +4 | -0.2 |  | +4 | V |
| Common-Mode Rejection Ratio (CMRR) | $\mathrm{V}_{\text {CM }}=0 \mathrm{~V}$ to 2 V | 66 | 80 |  | 69 | 80 |  | dB |
| $\mathrm{T}_{\text {min }}$ to $\mathrm{T}_{\text {max }}$ | $\mathrm{V}_{\mathrm{CM}}=0 \mathrm{~V}$ to 2 V | 66 |  |  | 66 |  |  | dB |


| Parameter | Condition | AD822 A Grade |  |  | AD822 B Grade |  |  | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Min | Typ | Max | Min | Typ | Max |  |
| Input Impedance |  | $10^{13} \mid 0.5$ |  |  |  |  |  |  |
| Differential |  |  |  |  | $\Omega \\| \mathrm{pF}$ |  |
| Common Mode |  | $10^{13}\| \| 2.8$ |  |  |  |  |  |  |  |  | $\Omega \\| \mathrm{pF}$ |
| OUTPUT CHARACTERISTICS |  |  |  |  |  |  |  |  |
| Output Saturation Voltage ${ }^{2}$ |  |  |  |  |  |  |  |  |
| $\mathrm{V}_{\text {OL }}-\mathrm{V}_{\text {EE }}$ | $\mathrm{I}_{\text {SINK }}=20 \mu \mathrm{~A}$ |  | 5 | 7 |  | 5 | 7 | mV |
| $\mathrm{T}_{\text {min }}$ to $\mathrm{T}_{\text {max }}$ |  |  |  | 10 |  |  | 10 | mV |
| $\mathrm{V}_{\text {cc }}-\mathrm{V}_{\text {or }}$ | $\mathrm{I}_{\text {SOURCE }}=20 \mu \mathrm{~A}$ |  | 10 | 14 |  | 10 | 14 | mV |
| $\mathrm{T}_{\text {min }}$ to $\mathrm{T}_{\text {max }}$ |  |  |  | 20 |  |  | 20 | mV |
| Vol - $\mathrm{V}_{\text {EE }}$ | $\mathrm{I}_{\text {SINK }}=2 \mathrm{~mA}$ |  | 40 | 55 |  | 40 | 55 | mV |
| $\mathrm{T}_{\text {min }}$ to $\mathrm{T}_{\text {max }}$ |  |  |  | 80 |  |  | 80 | mV |
| $\mathrm{V}_{\text {cc }}-\mathrm{V}_{\text {OH }}$ | $\mathrm{I}_{\text {SOURCE }}=2 \mathrm{~mA}$ |  | 80 | 110 |  | 80 | 110 | mV |
| $\mathrm{T}_{\text {MIN }}$ to $\mathrm{T}_{\text {MAX }}$ |  |  |  | 160 |  |  | 160 | mV |
| $V_{\text {OL- }} \mathrm{V}_{\text {EE }}$ | $\mathrm{I}_{\text {SINK }}=15 \mathrm{~mA}$ |  | 300 | 500 |  | 300 | 500 | mV |
| $\mathrm{T}_{\text {min }}$ to $\mathrm{T}_{\text {max }}$ |  |  |  | 1000 |  |  | 1000 | mV |
| $\mathrm{V}_{\text {cc }}-\mathrm{V}_{\text {OH }}$ | $\mathrm{I}_{\text {SOURCE }}=15 \mathrm{~mA}$ |  | 800 | 1500 |  | 800 | 1500 | mV |
| $\mathrm{T}_{\text {min }}$ to $\mathrm{T}_{\text {max }}$ |  |  |  | 1900 |  |  | 1900 | mV |
| Operating Output Current |  | 15 |  |  | 15 |  |  | mA |
| $\mathrm{T}_{\text {min }}$ to $\mathrm{T}_{\text {max }}$ |  | 12 |  |  | 12 |  |  | $\mathrm{mA}$ |
| Capacitive Load Drive |  |  | 350 |  |  | 350 |  | pF |
| POWER SUPPLY |  |  |  |  |  |  |  |  |
| Quiescent Current $\mathrm{T}_{\text {MIN }}$ to $\mathrm{T}_{\text {MAX }}$ |  |  | 1.24 | 1.6 |  | 1.24 | 1.6 | mA |
| Power Supply Rejection | $\mathrm{V}_{\mathrm{s}}+=5 \mathrm{~V}$ to 15 V | 66 | 80 |  | 70 | 80 |  | dB |
| $\mathrm{T}_{\text {MIN }}$ to $\mathrm{T}_{\text {MAX }}$ |  | 66 |  |  | 70 |  |  | dB |

${ }^{1}$ This is a functional specification. Amplifier bandwidth decreases when the input common-mode voltage is driven in the range (+ $\left.\mathrm{V}_{s}-1 \mathrm{~V}\right)$ to $+\mathrm{V}_{s}$. Common-mode effort voltage is typically less than 5 mV with the common-mode voltage set at 1 V below the positive supply.
${ }^{2} \mathrm{~V}_{\mathrm{OL}}-\mathrm{V}_{\mathrm{EE}}$ is defined as the difference between the lowest possible output voltage $\left(\mathrm{V}_{\mathrm{OL}}\right)$ and the negative voltage supply rail ( $\mathrm{V}_{\mathrm{EE}}$ ). $\mathrm{V}_{\mathrm{CC}}-\mathrm{V}_{\mathrm{OH}}$ is defined as the difference between the highest possible output voltage $\left(\mathrm{V}_{\text {OH }}\right)$ and the positive supply voltage $\left(\mathrm{V}_{\mathrm{Cc}}\right)$.
$\mathrm{V}_{\mathrm{S}}= \pm 5 \mathrm{~V} @ \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{CM}}=0 \mathrm{~V}, \mathrm{~V}_{\text {out }}=0 \mathrm{~V}$, unless otherwise noted.
Table 2.

| Parameter | Conditions | AD822 A Grade |  |  | AD822 B Grade |  |  | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Min | Typ | Max | Min | Typ | Max |  |
| DC PERFORMANCE |  |  |  |  |  |  |  |  |
| Initial Offset |  |  | 0.1 | 0.8 |  | 0.1 | 0.4 | mV |
| Maximum Offset Overtemperature |  |  | 0.5 | 1.5 |  | 0.5 | 1 | mV |
| Offset Drift |  |  | 2 |  |  | 2 |  | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
| Input Bias Current | $V_{C M}=-5 \mathrm{~V}$ to +4 V |  | 2 | 25 |  | 2 | 10 | PA |
| at Tmax |  |  | 0.5 | 5 |  | 0.5 | 2.5 | nA |
| Input Offset Current |  |  | 2 | 20 |  | 2 | 10 | pA |
| at $\mathrm{T}_{\text {max }}$ |  |  | 0.5 |  |  | 0.5 |  | nA |
| Open-Loop Gain | $\mathrm{V}_{\mathrm{o}}=-4 \mathrm{~V}$ to +4 V |  |  |  |  |  |  |  |
|  | $\mathrm{RL}=100 \mathrm{k} \Omega$ | 400 | 1000 |  | 400 | 1000 |  | $\mathrm{V} / \mathrm{mV}$ |
| $\mathrm{T}_{\text {min }}$ to $\mathrm{T}_{\text {max }}$ |  | 400 |  |  | 400 |  |  | $\mathrm{V} / \mathrm{mV}$ |
|  | $\mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega$ | 80 | 150 |  | 80 | 150 |  | $\mathrm{V} / \mathrm{mV}$ |
| $\mathrm{T}_{\text {min }}$ to $\mathrm{T}_{\text {max }}$ |  | 80 |  |  | 80 |  |  | $\mathrm{V} / \mathrm{mV}$ |
|  | $\mathrm{R}_{\mathrm{L}}=1 \mathrm{k} \Omega$ |  | 30 |  | 20 | 30 |  | $\mathrm{V} / \mathrm{mV}$ |
| $\mathrm{T}_{\text {MIN }}$ to $\mathrm{T}_{\text {MAX }}$ |  | 10 |  |  | 10 |  |  | $\mathrm{V} / \mathrm{mV}$ |

## AD822



${ }^{1}$ This is a functional specification. Amplifier bandwidth decreases when the input common-mode voltage is driven in the range ( $+\mathrm{V}_{s}-1 \mathrm{~V}$ ) to $+\mathrm{V}_{s}$. Common-mode effort voltage is typically less than 5 mV with the common-mode voltage set at 1 V below the positive supply.
${ }^{2} \mathrm{~V}_{\mathrm{OL}}-\mathrm{V}_{E E}$ is defined as the difference between the lowest possible output voltage $\left(\mathrm{V}_{\mathrm{OL}}\right)$ and the negative voltage supply rail ( $\mathrm{V}_{\mathrm{EE}}$ ). $\mathrm{V}_{\mathrm{CC}}-\mathrm{V}_{\mathrm{OH}}$ is defined as the difference between the highest possible output voltage $\left(\mathrm{V}_{\mathrm{OH}}\right)$ and the positive supply voltage $\left(\mathrm{V}_{\mathrm{Cc}}\right)$.
$\mathrm{V}_{\mathrm{S}}= \pm 15 \mathrm{~V} @ \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{CM}}=0 \mathrm{~V}, \mathrm{~V}_{\text {out }}=0 \mathrm{~V}$, unless otherwise noted.
Table 3.

| Parameter | Conditions | AD822 A Grade |  |  | AD822 B Grade |  |  | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Min | Typ | Max | Min | Typ | Max |  |
| DC PERFORMANCE |  |  |  |  |  |  |  |  |
| Initial Offset |  |  | 0.4 | 2 |  | 0.3 | 1.5 | mV |
| Maximum Offset Overtemperature |  |  | 0.5 | 3 |  | 0.5 | 2.5 | mV |
| Offset Drift |  |  | 2 |  |  | 2 |  | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
| Input Bias Current | $\mathrm{V}_{\text {cm }}=0 \mathrm{~V}$ |  |  | 25 |  | 2 | 12 | pA |
|  | $V_{\text {CM }}=-10 \mathrm{~V}$ |  | 40 |  |  | 40 |  | pA |
| at $\mathrm{T}_{\text {max }}$ | $\mathrm{V}_{\text {cm }}=0 \mathrm{~V}$ |  | 0.5 | 5 |  | 0.5 | 2.5 | nA |
| Input Offset Current |  |  | 2 | 20 |  | 2 | 12 | pA |
| at $\mathrm{T}_{\text {max }}$ |  |  | 0.5 |  |  | 0.5 |  | nA |
| Open-Loop Gain | $\mathrm{V}_{0}=+10 \mathrm{~V}$ to -10 V |  |  |  |  |  |  |  |
| $\mathrm{R}_{\mathrm{L}}=100 \mathrm{k} \Omega$ | 500 | 2000 |  | 500 | 2000 |  |  | $\mathrm{V} / \mathrm{mV}$ |
| $\mathrm{T}_{\text {min }}$ to $\mathrm{T}_{\text {max }}$ |  | 500 |  |  | 500 |  |  | $\mathrm{V} / \mathrm{mV}$ |
| $\mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega$ | 100 | 500 |  | 100 | 500 |  |  | $\mathrm{V} / \mathrm{mV}$ |
| $\mathrm{T}_{\text {min }}$ to $\mathrm{T}_{\text {max }}$ |  | 100 |  |  | 100 |  |  | $\mathrm{V} / \mathrm{mV}$ |
| $\mathrm{R}_{\mathrm{L}}=1 \mathrm{k} \Omega$ | 30 | 45 |  | 30 | 45 |  |  | $\mathrm{V} / \mathrm{mV}$ |
| $\mathrm{T}_{\text {min }}$ to $\mathrm{T}_{\text {max }}$ |  | 20 |  |  | 20 |  |  | $\mathrm{V} / \mathrm{mV}$ |
| NOISE/HARMONIC PERFORMANCE Input Voltage Noise |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |
| 0.1 Hz to 10 Hz |  |  | 2 |  |  | 2 |  | $\mu \mathrm{V}$ p-p |
| $f=10 \mathrm{~Hz}$ |  |  | 25 |  |  | 25 |  | $\mathrm{nV} / \sqrt{ } \mathrm{Hz}$ |
| $\mathrm{f}=100 \mathrm{~Hz}$ |  |  | 21 |  |  | 21 |  | $\mathrm{nV} / \sqrt{ } \mathrm{Hz}$ |
| $\mathrm{f}=1 \mathrm{kHz}$ |  |  | 16 |  |  | 16 |  | $\mathrm{nV} / \sqrt{ } \mathrm{Hz}$ |
| $\mathrm{f}=10 \mathrm{kHz}$ |  |  | 13 |  |  | 13 |  | $\mathrm{nV} / \sqrt{ } \mathrm{Hz}$ |
| Input Current Noise |  |  |  |  |  |  |  |  |
| 0.1 Hz to 10 Hz |  |  | 18 |  |  | 18 |  | fA p-p |
| $\mathrm{f}=1 \mathrm{kHz}$ |  |  | 0.8 |  |  | 0.8 |  | $\mathrm{fA} / \sqrt{ } \mathrm{Hz}$ |
| Harmonic Distortion | $\mathrm{RL}=10 \mathrm{k} \Omega$ |  |  |  |  |  |  |  |
| $\mathrm{f}=10 \mathrm{kHz}$ | $\mathrm{V}_{\mathrm{O}}= \pm 10 \mathrm{~V}$ |  | -85 |  |  | -85 |  | dB |
| DYNAMIC PERFORMANCE |  |  |  |  |  |  |  |  |
| Unity Gain Frequency |  |  | 1.9 |  |  | 1.9 |  | MHz |
| Full Power Response | Vop-p $=20 \mathrm{~V}$ |  | 45 |  |  | 45 |  | kHz |
| Slew Rate |  |  | 3 |  |  | 3 |  | V/ $/ \mathrm{s}$ |
| Settling Time |  |  |  |  |  |  |  |  |
| to $0.1 \%$ | $\mathrm{V}_{\mathrm{o}}=0 \mathrm{~V}$ to $\pm 10 \mathrm{~V}$ |  | 4.1 |  |  | 4.1 |  | $\mu \mathrm{s}$ |
| to 0.01\% |  |  | 4.5 |  |  | 4.5 |  | $\mu \mathrm{s}$ |

## AD822

| Parameter | Conditions | AD822 A Grade |  |  | AD822 B Grade |  |  | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Min | Typ | Max | Min | Typ | Max |  |
| MATCHING CHARACTERISTICS |  |  |  |  |  |  |  |  |
| Initial Offset |  |  |  | 3 |  |  | 2 | mV |
| Maximum Offset Overtemperature |  |  |  | 4 |  |  | 2.5 | mV |
| Offset Drift |  |  | 3 |  |  | 3 |  | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
| Input Bias Current |  |  |  | 25 |  |  | 12 | pA |
| Crosstalk @ f= 1 kHz | $\mathrm{RL}=5 \mathrm{k} \Omega$ |  | -130 |  |  | -130 |  | dB |
| $\mathrm{f}=100 \mathrm{kHz}$ |  |  | -93 |  |  | -93 |  | dB |
| INPUT CHARACTERISTICS |  |  |  |  |  |  |  |  |
| Input Voltage Range ${ }^{1}$ |  | -15.2 |  | +14 | -15.2 |  | +4 | V |
| $\mathrm{T}_{\text {min }}$ to $\mathrm{T}_{\text {max }}$ |  | -15.2 |  | +14 | -15.2 |  | +4 | V |
| Common-Mode Rejection Ratio (CMRR) | $\mathrm{V}_{\text {CM }}=-15 \mathrm{~V}$ to +12 V | 70 | 80 |  | 74 | 90 |  | dB |
| $\mathrm{T}_{\text {Min }}$ to $\mathrm{T}_{\text {Max }}$ | $\mathrm{V}_{\mathrm{CM}}=-15 \mathrm{~V}$ to +12 V |  | 70 |  |  | 74 |  | dB |
| Input Impedance |  |  |  |  |  |  |  |  |
| Differential |  |  | $10^{13}\| \| 0.5$ |  |  | $10^{13}\| \| 0.5$ |  | $\Omega \\| \mathrm{pF}$ |
| Common Mode |  |  | $10^{13}\| \| 2.8$ |  |  | $10^{13}\| \| 2.8$ |  | $\Omega \\| \mathrm{pF}$ |
| OUTPUT CHARACTERISTICS |  |  |  |  |  |  |  |  |
| Output Saturation Voltage ${ }^{2}$ |  |  |  |  |  |  |  |  |
| VoL - $\mathrm{V}_{\text {EE }}$ | $\mathrm{I}_{\text {SINK }}=20 \mu \mathrm{~A}$ |  | 5 | 7 |  | 5 | 7 | mV |
| $\mathrm{T}_{\text {min }}$ to $\mathrm{T}_{\text {max }}$ |  |  |  | 10 |  |  | 10 | mV |
| $\mathrm{V}_{\text {cc }}-\mathrm{V}_{\text {OH }}$ | $\mathrm{I}_{\text {SOURCE }}=20 \mu \mathrm{~A}$ |  | 10 | 14 |  | 10 | 14 | mV |
| $\mathrm{T}_{\text {min }}$ to $\mathrm{Tmax}^{\text {max }}$ |  |  |  | 20 |  |  | 20 | mV |
| $\mathrm{V}_{\mathrm{OL}}-\mathrm{V}_{\text {EE }}$ | $\mathrm{ISINK}=2 \mathrm{~mA}$ |  | 40 | 55 |  | 40 | 55 | mV |
| $\mathrm{T}_{\text {min }}$ to $\mathrm{T}_{\text {max }}$ |  |  |  | 80 |  |  | 80 | mV |
| $\mathrm{V}_{\text {cc }}-\mathrm{V}_{\text {oH }}$ | $\mathrm{I}_{\text {SOURCE }}=2 \mathrm{~mA}$ |  | 80 | 110 |  | 80 | 110 | mV |
| $\mathrm{Tmin}_{\text {to }} \mathrm{T}_{\text {max }}$ |  |  |  | 160 |  |  | 160 | mV |
| $\mathrm{V}_{\text {ol }}$ - $\mathrm{V}_{\text {Ee }}$ | $\mathrm{I}_{\mathrm{SINK}}=15 \mathrm{~mA}$ |  | 300 | 500 |  | 300 | 500 | mV |
| $\mathrm{T}_{\text {min }}$ to $\mathrm{T}_{\text {max }}$ |  |  |  | 1000 |  |  | 1000 | mV |
| $\mathrm{V}_{\text {cc }}-\mathrm{V}_{\text {OH }}$ | $I_{\text {SoURCE }}=15 \mathrm{~mA}$ |  | 800 | 1500 |  | 800 | 1500 | mV |
| $\mathrm{T}_{\text {min }}$ to $\mathrm{T}_{\text {max }}$ |  |  |  | 1900 |  |  | 1900 | mV |
| Operating Output Current |  | 20 |  |  | 20 |  |  | mA |
| $\mathrm{T}_{\text {min }}$ to $\mathrm{T}_{\text {max }}$ |  | 15 |  |  | 15 |  |  | mA |
| Capacitive Load Drive |  |  | 350 |  |  | 350 |  | pF |
| POWER SUPPLY |  |  |  |  |  |  |  |  |
| Quiescent Current $\mathrm{T}_{\text {Min }}$ to $\mathrm{T}_{\text {MAX }}$ |  |  | 1.4 | 18 |  | 1.4 | 1.8 | mA |
| Power Supply Rejection | $\mathrm{V}_{\mathrm{s}}+=5 \mathrm{~V}$ to 15 V | 70 | 80 |  | 70 | 80 |  | dB |
| $\mathrm{T}_{\text {min }}$ to $\mathrm{Tmax}^{\text {max }}$ |  | 70 |  |  | 70 |  |  | dB |

${ }^{1}$ This is a functional specification. Amplifier bandwidth decreases when the input common-mode voltage is driven in the range (+ $\left.\mathrm{V}_{s}-1 \mathrm{~V}\right)$ to $+\mathrm{V}_{s}$. Common-mode effort voltage is typically less than 5 mV with the common-mode voltage set at 1 V below the positive supply.
${ }^{2} V_{O L}-V_{E E}$ is defined as the difference between the lowest possible output voltage ( $V_{O L}$ ) and the negative voltage supply rail ( $\mathrm{V}_{\mathrm{EE}}$ ). $\mathrm{V}_{\mathrm{CC}}-\mathrm{V}_{\mathrm{OH}}$ is defined as the difference between the highest possible output voltage ( $\mathrm{V}_{\text {or }}$ ) and the positive supply voltage ( $\mathrm{V}_{\text {cc }}$ ).
$\mathrm{V}_{\mathrm{S}}=0,3 \mathrm{~V} @ \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{CM}}=0 \mathrm{~V}, \mathrm{~V}$ out $=0.2 \mathrm{~V}$, unless otherwise noted.
Table 4.

| Parameter | Conditions | Typ | Unit |
| :--- | :--- | :--- | :--- |
| DC PERFORMANCE |  |  |  |
| Initial Offset |  | 0.2 | mV |
| Maximum Offset Overtemperature |  | 0.5 | mV |
| Offset Drift | $V_{C M}=0$ V to 2 V | 1 | $\mu \mathrm{C} /{ }^{\circ} \mathrm{C}$ |
| Input Bias Current |  | 2 | pA |
| $\quad$ at $T_{\text {MAX }}$ |  | 0.5 | nA |
| Input Offset Current |  | 2 | pA |
| at $T_{\text {MAX }}$ |  | 0.5 | nA |


| Parameter | Conditions | Typ | Unit |
| :---: | :---: | :---: | :---: |
| Open-Loop Gain $\begin{aligned} & \mathrm{R}_{\mathrm{L}}=100 \mathrm{k} \Omega \\ & \mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega \\ & \mathrm{R}_{\mathrm{L}}=1 \mathrm{k} \Omega \end{aligned}$ | $\mathrm{V}_{\mathrm{o}}=0.2 \mathrm{~V}$ to 2 V | $\begin{aligned} & 1000 \\ & 150 \\ & 30 \end{aligned}$ | $\begin{aligned} & \mathrm{V} / \mathrm{mV} \\ & \mathrm{~V} / \mathrm{mV} \\ & \mathrm{~V} / \mathrm{mV} \end{aligned}$ |
| NOISE/HARMONIC PERFORMANCE Input Voltage Noise 0.1 Hz to 10 Hz $\mathrm{f}=10 \mathrm{~Hz}$ $\mathrm{f}=100 \mathrm{~Hz}$ $\mathrm{f}=1 \mathrm{kHz}$ $\mathrm{f}=10 \mathrm{kHz}$ <br> Input Current Noise 0.1 Hz to 10 Hz $\mathrm{f}=1 \mathrm{kHz}$ <br> Harmonic Distortion $\mathrm{f}=10 \mathrm{kHz}$ | $\begin{aligned} & \mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega \text { to } 1.5 \mathrm{~V} \\ & \mathrm{~V}_{\mathrm{O}}= \pm 1.25 \mathrm{~V} \end{aligned}$ | $\begin{aligned} & 2 \\ & 25 \\ & 21 \\ & 16 \\ & 13 \\ & \\ & 18 \\ & 0.8 \\ & \\ & -92 \\ & \hline \end{aligned}$ | $\mu \mathrm{V}$ p-p <br> $\mathrm{nV} / \sqrt{ } \mathrm{Hz}$ <br> $\mathrm{nV} / \sqrt{ } \mathrm{Hz}$ <br> $\mathrm{nV} / \sqrt{ } \mathrm{Hz}$ <br> $\mathrm{nV} / \sqrt{ } \mathrm{Hz}$ <br> fA p-p fA/ $\sqrt{\mathrm{Hz}}$ <br> dB |
| DYNAMIC PERFORMANCE <br> Unity Gain Frequency <br> Full Power Response <br> Slew Rate <br> Settling Time <br> to $0.1 \%$ <br> to $0.01 \%$ | $V_{o} p-p=2.5 \mathrm{~V}$ $\mathrm{V}_{\mathrm{o}}=0.2 \mathrm{~V} \text { to } 2.5 \mathrm{~V}$ | $\begin{aligned} & 1.5 \\ & 240 \\ & 3 \\ & 1 \\ & 1.4 \end{aligned}$ | MHz <br> kHz <br> V/ $\mu \mathrm{s}$ <br> $\mu \mathrm{s}$ <br> $\mu \mathrm{s}$ |
| ```MATCHING CHARACTERISTICS Offset Drift Crosstalk @f=1 kHz f=100 kHz``` | R L $=5 \mathrm{k} \Omega$ | $\begin{aligned} & 2 \\ & -130 \\ & -93 \end{aligned}$ | $\begin{aligned} & \mu \mathrm{V} /{ }^{\circ} \mathrm{C} \\ & \mathrm{~dB} \\ & \mathrm{~dB} \end{aligned}$ |
| INPUT CHARACTERISTICS <br> Common-Mode Rejection Ratio (CMRR) Input Impedance <br> Differential <br> Common Mode | $\mathrm{V}_{\text {cm }}=0 \mathrm{~V}$ to 1 V | 74 <br> $10^{13}\| \| 0.5$ <br> $10^{13}\| \| 2.8$ | dB <br> $\Omega \\| p F$ <br> $\Omega \\| p F$ |
| OUTPUT CHARACTERISTICS <br> Output Saturation Voltage ${ }^{1}$ $\begin{aligned} & \mathrm{V}_{\mathrm{OL}}-\mathrm{V}_{\mathrm{EE}} \\ & \mathrm{~V}_{\mathrm{CC}}-\mathrm{V}_{\mathrm{OH}} \\ & \mathrm{~V}_{\mathrm{OL}}-\mathrm{V}_{\mathrm{EE}} \\ & \mathrm{~V}_{\mathrm{CC}}-\mathrm{V}_{\mathrm{OH}} \\ & \mathrm{~V}_{\mathrm{OL}}-\mathrm{V}_{\mathrm{EE}} \\ & \mathrm{~V}_{\mathrm{CC}}-\mathrm{V}_{\mathrm{OH}} \end{aligned}$ <br> Capacitive Load Drive | $\begin{aligned} & I_{\text {SINK }}=20 \mu \mathrm{~A} \\ & I_{\text {SOURCE }}=20 \mu \mathrm{~A} \\ & I_{\text {SIINK }}=2 \mathrm{~mA} \\ & I_{\text {SOURCE }}=2 \mathrm{~mA} \\ & I_{\text {SIINK }}=10 \mathrm{~mA} \\ & I_{\text {SOURCE }}=10 \mathrm{~mA} \end{aligned}$ | $\begin{aligned} & 5 \\ & 10 \\ & 40 \\ & 80 \\ & 200 \\ & 500 \\ & 350 \\ & \hline \end{aligned}$ | mV <br> mV <br> mV <br> mV <br> mV <br> mV <br> pF |
| POWER SUPPLY <br> Quiescent Current Power Supply Rejection | $\mathrm{V}_{\mathrm{s}}+=3 \mathrm{~V}$ to 15 V | $\begin{aligned} & 1.24 \\ & 80 \end{aligned}$ | $\begin{aligned} & \mathrm{mA} \\ & \mathrm{~dB} \end{aligned}$ |

${ }^{1} V_{O L}-V_{E E}$ is defined as the difference between the lowest possible output voltage $\left(V_{O L}\right)$ and the negative voltage supply rail ( $V_{E E}$ ). $V_{C C}-V_{O H}$ is defined as the difference between the highest possible output voltage $\left(\mathrm{V}_{\text {он }}\right)$ and the positive supply voltage $\left(\mathrm{V}_{\mathrm{cc}}\right)$.

## ABSOLUTE MAXIMUM RATINGS

Table 5.

| Parameter | Rating |
| :---: | :---: |
| Supply Voltage | $\pm 18 \mathrm{~V}$ |
| Internal Power Dissipation ${ }^{1}$ |  |
| PDIP (N) | Observe Derating Curves |
| SOIC (R) | Observe Derating Curves |
| Input Voltage | $\begin{aligned} & \left(+\mathrm{V}_{\mathrm{s}}+0.2 \mathrm{~V}\right) \text { to } \\ & -\left(20 \mathrm{~V}+\mathrm{V}_{\mathrm{s}}\right) \end{aligned}$ |
| Output Short Circuit Duration | Indefinite |
| Differential Input Voltage | $\pm 30 \mathrm{~V}$ |
| Storage Temperature Range (N) | $-65^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |
| Storage Temperature Range (R, RM) | $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| Operating Temperature Range |  |
| AD822 A Grade and B Grade | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
| Lead Temperature Range (Soldering, 60 sec ) | $260^{\circ} \mathrm{C}$ |

[^0]Stresses above those listed under Absolute Maximum Ratings may cause permanent damage to the device. This is a stress rating only; functional operation of the device at these or any other conditions above those indicated in the operational section of this specification is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

## MAXIMUM POWER DISSIPATION

The maximum power that can be safely dissipated by the AD822 is limited by the associated rise in junction temperature. For plastic packages, the maximum safe junction temperature is $145^{\circ} \mathrm{C}$. If these maximums are exceeded momentarily, proper circuit operation is restored as soon as the die temperature is reduced. Leaving the device in the overheated condition for an extended period can result in device burnout. To ensure proper operation, it is important to observe the derating curves shown in Figure 27.

While the AD822 is internally short circuit protected, this may not be sufficient to guarantee that the maximum junction temperature is not exceeded under all conditions. With power supplies $\pm 12 \mathrm{~V}$ (or less) at an ambient temperature of $25^{\circ} \mathrm{C}$ or less, if the output node is shorted to a supply rail, then the amplifier is not destroyed, even if this condition persists for an extended period.

## ESD CAUTION

ESD (electrostatic discharge) sensitive device. Electrostatic charges as high as 4000 V readily accumulate on the human body and test equipment and can discharge without detection. Although this product features proprietary ESD protection circuitry, permanent damage may occur on devices subjected to high energy electrostatic discharges. Therefore, proper ESD precautions are recommended to avoid performance degradation or loss of functionality.


## TYPICAL PERFORMANCE CHARACTERISTICS



Figure 4. Typical Distribution of Offset Voltage (390 Units)


Figure 5. Typical Distribution of Offset Voltage Drift (100 Units)


Figure 6. Typical Distribution of Input Bias Current (213 Units)


Figure 7. Input Bias Current vs. Common-Mode Voltage; $V_{s}=5 \mathrm{~V}, 0 \mathrm{~V}$, and $V_{s}= \pm 5 \mathrm{~V}$


Figure 8. Input Bias Current vs. Common-Mode Voltage; $V_{s}= \pm 15 \mathrm{~V}$


Figure 9. Input Bias Current vs. Temperature; $V_{S}=5 \mathrm{~V}, V_{C M}=0$

## AD822



Figure 10. Open-Loop Gain vs. Load Resistance


Figure 11. Open-Loop Gain vs. Temperature


Figure 12. Input Error Voltage vs. Output Voltage for Resistive Loads


Figure 13. Input Effort Voltage with Output Voltage Within 300 mV of Either Supply Rail for Various Resistive Loads; $V_{s}= \pm 5 \mathrm{~V}$


Figure 14. Input Voltage Noise vs. Frequency


Figure 15. Total Harmonic Distortion (THD) vs. Frequency


Figure 16. Open-Loop Gain and Phase Margin vs. Frequency


Figure 17. Output Impedance vs. Frequency


Figure 18. Output Swing and Error vs. Settling Time


Figure 19. Common-Mode Rejection vs. Frequency


Figure 20. Absolute Common-Mode Error vs. Common-Mode Voltage from Supply Rails (Vs - VCM)


Figure 21. Output Saturation Voltage vs. Load Current


Figure 22. Output Saturation Voltage vs. Temperature


Figure 23. Short Circuit Current Limit vs. Temperature


Figure 24. Quiescent Current vs. Supply Voltage vs. Temperature


Figure 25. Power Supply Rejection vs. Frequency


Figure 26. Large Signal Frequency Response


Figure 27. Maximum Power Dissipation vs. Temperature for Packages


Figure 28. Crosstalk vs. Frequency


Figure 29. Unity Gain Follower


Figure 30. $20 \mathrm{~V} p-\mathrm{p}, 25 \mathrm{kHz}$ Sine Wave Input; Unity Gain Follower; $R_{L}=600 \Omega$, $V_{s}= \pm 15 \mathrm{~V}$


Figure 31. Crosstalk Test Circuit


Figure 32. Large Signal Response Unity Gain Follower; $V_{S}= \pm 15 \mathrm{~V}, R_{L}=10 \mathrm{k} \Omega$


Figure 33. Small Signal Response Unity Gain Follower; $V_{S}= \pm 15 \mathrm{~V}, R_{L}=10 \mathrm{k} \Omega$


Figure 34. Vs $=5 \mathrm{~V}, 0 \mathrm{~V}$; Unity Gain Follower Response to 0 V to 4 V Step


Figure 35. Unity Gain Follower


Figure 36. Gain-of-T2 Inverter


Figure 37. Vs $=5 \mathrm{~V}, 0 \mathrm{~V}$; Unity Gain Follower Response to 0 V to 5 V Step


Figure 38. V $=5 \mathrm{~V}, 0 \mathrm{~V}$; Unity Gain Follower Response to 40 mV Step, Centered 40 mV above Ground, $R_{L}=10 \mathrm{k} \Omega$


Figure 39. Vs $=5 \mathrm{~V}, 0 \mathrm{~V}$; Gain-of-2 Inverter Response to 20 mV Step, Centered 20 mV below Ground, $R_{L}=10 \mathrm{k} \Omega$


Figure 40. V $=5 \mathrm{~V}, 0 \mathrm{~V}$; Gain-of-2 Inverter Response to 2.5 V Step, Centered -1.25 V below Ground, $R_{L}=10 \mathrm{k} \Omega$


Figure 41. V $=3$ V, 0 V; Gain-of-2 Inverter, $V_{I N}=1.25 \mathrm{~V}, 25 \mathrm{kHz}$, Sine Wave Centered at $-0.75 \mathrm{~V}, R_{L}=600 \Omega$

(a)

(b)


Figure 42. (a) Response with $R_{P}=0 ; V_{I N}$ from 0 to $+V_{s}$
(b) $V_{I N}=0$ to $+V_{s}+200 \mathrm{mV}$
$V_{\text {OUT }}=0$ to $+V_{S}$
$R_{P}=49.9 \mathrm{k} \Omega$

## AD822

## APPLICATION NOTES

## InPUT ChARACTERIITICS

In the AD822, n -channel JFETs are used to provide a low offset, low noise, high impedance input stage. Minimum input common-mode voltage extends from 0.2 V below $-\mathrm{V}_{\mathrm{S}}$ to 1 V less than $+\mathrm{V}_{\mathrm{s}}$. Driving the input voltage closer to the positive rail causes a loss of amplifier bandwidth (as can be seen by comparing the large signal responses shown in Figure 34 and Figure 37) and increased common-mode voltage error as illustrated in Figure 20.

The AD822 does not exhibit phase reversal for input voltages up to and including +V s. Figure 42 shows the response of an AD822 voltage follower to a 0 V to $5 \mathrm{~V}(+\mathrm{V})$ square wave input. The input and output are superimposed. The output tracks the input up to $+V_{s}$ without phase reversal. The reduced bandwidth above a 4 V input causes the rounding of the output waveform. For input voltages greater than $+V_{s}$, a resistor in series with the AD822's noninverting input prevents phase reversal, at the expense of greater input voltage noise. This is illustrated in Figure 42.

Since the input stage uses n-channel JFETs, input current during normal operation is negative; the current flows out from the input terminals. If the input voltage is driven more positive than $+\mathrm{V}_{\mathrm{s}}-0.4 \mathrm{~V}$, then the input current reverses direction as internal device junctions become forward biased. This is illustrated in Figure 7.

A current limiting resistor should be used in series with the input of the AD822 if there is a possibility of the input voltage exceeding the positive supply by more than 300 mV , or if an input voltage is applied to the AD 822 when $\pm \mathrm{V}_{\mathrm{S}}=0$. The amplifier is damaged if left in that condition for more than 10 seconds. A $1 \mathrm{k} \Omega$ resistor allows the amplifier to withstand up to 10 V of continuous overvoltage and increases the input voltage noise by a negligible amount.

Input voltages less than $-\mathrm{V}_{\mathrm{s}}$ are a completely different story. The amplifier can safely withstand input voltages 20 V below the negative supply voltage as long as the total voltage from the positive supply to the input terminal is less than 36 V . In addition, the input stage typically maintains picoampere (pA) level input currents across that input voltage range.

The AD822 is designed for $13 \mathrm{nV} / \sqrt{ } \mathrm{Hz}$ wideband input voltage noise and maintains low noise performance to low frequencies (refer to Figure 14). This noise performance, along with the AD822's low input current and current noise, means that the AD822 contributes negligible noise for applications with source resistances greater than $10 \mathrm{k} \Omega$ and signal bandwidths greater than 1 kHz . This is illustrated in Figure 43.


Figure 43. Total Noise vs. Source Impedance

## OUTPUT CHARACTERISTICS

The AD822's unique bipolar rail-to-rail output stage swings within 5 mV of the negative supply and 10 mV of the positive supply with no external resistive load. The AD822's approximate output saturation resistance is $40 \Omega$ sourcing and $20 \Omega$ sinking. This can be used to estimate output saturation voltage when driving heavier current loads. For instance, when sourcing 5 mA , the saturation voltage to the positive supply rail is 200 mV ; when sinking 5 mA , the saturation voltage to the negative rail is 100 mV .

The amplifier's open-loop gain characteristic changes as a function of resistive load, as shown in Figure 10 to Figure 13. For load resistances over $20 \mathrm{k} \Omega$, the AD822's input error voltage is virtually unchanged until the output voltage is driven to 180 mV of either supply.

If the AD822's output is overdriven so as to saturate either of the output devices, the amplifier recovers within $2 \mu$ s of its input returning to the amplifier's linear operating region.

Direct capacitive loads interact with the amplifier's effective output impedance to form an additional pole in the amplifier's feedback loop, which can cause excessive peaking on the pulse response or loss of stability. Worst case is when the amplifier is used as a unity gain follower. Figure 44 shows the AD822's pulse response as a unity gain follower driving 350 pF . This amount of overshoot indicates approximately $20^{\circ}$ of phase margin-the system is stable, but nearing the edge. Configurations with less loop gain, and as a result less loop bandwidth, are much less sensitive to capacitance load effects.


Figure 44. Small Signal Response of AD822 as Unity Gain Follower Driving 350 pF

Figure 45 is a plot of capacitive load that results in a $20^{\circ}$ phase margin vs. noise gain for the AD822. Noise gain is the inverse of the feedback attenuation factor provided by the feedback network in use.



哭
$\vdots$
高
Figure 45. Capacitive Load Tolerance vs. Noise Gain

Figure 46 shows a method for extending capacitance load drive capability for a unity gain follower. With these component values, the circuit drives 5000 pF with a $10 \%$ overshoot.


Figure 46. Extending Unity Gain Follower Capacitive Load Capability Beyond 350 pF

## APPLICATIONS

## SINGLE-SUPPLY VOLTAGE-TO-FREQUENCY CONVERTER

The circuit shown in Figure 47 uses the AD822 to drive a low power timer that produces a stable pulse of width $t_{1}$. The positive going output pulse is integrated by $\mathrm{R} 1-\mathrm{C} 1$ and used as one input to the AD822 that is connected as a differential integrator. The other input (nonloading) is the unknown voltage, $\mathrm{V}_{\text {IN }}$. The AD822 output drives the timer trigger input, closing the overall feedback loop.


Figure 47. Single-Supply Voltage-to-Frequency Converter
Typical AD822 bias currents of 2 pA allow $\mathrm{M} \Omega$ range source impedances with negligible dc errors. Linearity errors on the order of $0.01 \%$ full scale can be achieved with this circuit. This performance is obtained with a 5 V single supply that delivers less than 1 mA to the entire circuit.

## SINGLE-SUPPLY PROGRAMMABLE GAIN INSTRUMENTATION AMPLIFIER

The AD822 can be configured as a single-supply instrumentation amplifier that is able to operate from single supplies down to 3 V or dual supplies up to $\pm 15 \mathrm{~V}$. Using only one AD822 rather than three separate op amps, this circuit is cost and power efficient. The AD822 FET inputs' 2 pA bias currents minimize offset errors caused by high unbalanced source impedances.

An array of precision thin-film resistors sets the in amp gain to be either 10 or 100 . These resistors are laser trimmed to ratio match to $0.01 \%$ and have a maximum differential TC of $5 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$.

Table 6. In Amp Performance


Figure 48. Pulse Response of In Amp to a 500 mV p-p Input Signal; $V_{s}=5 \mathrm{~V}$, 0 V ; Gain = 0


Figure 49. A Single-Supply Programmable Instrumentation Amplifier

## 3 V, SINGLE-SUPPLY STEREO HEADPHONE DRIVER

The AD822 exhibits good current drive and THD + N performance, even at 3 V single supplies. At 1 kHz , total harmonic distortion plus noise (THD +N ) equals -62 dB ( $0.079 \%$ ) for a 300 mV p-p output signal. This is comparable to other single-supply op amps that consume more power and cannot run on 3 V power supplies.


Figure 50. 3 V Single-Supply Stereo Headphone Driver
In Figure 50, each channel's input signal is coupled via a $1 \mu \mathrm{~F}$ Mylar capacitor. Resistor dividers set the dc voltage at the noninverting inputs so that the output voltage is midway between the power supplies ( 1.5 V ). The gain is 1.5 . Each half of the AD822 can then be used to drive a headphone channel. A 5 Hz high-pass filter is realized by the $500 \mu \mathrm{~F}$ capacitors and the headphones that can be modeled as $32 \Omega$ load resistors to ground. This ensures that all signals in the audio frequency range $(20 \mathrm{~Hz}$ to 20 kHz$)$ are delivered to the headphones.

## LOW DROPOUT BIPOLAR BRIDGE DRIVER

The AD822 can be used for driving a $350 \Omega$ Wheatstone bridge. Figure 51 shows one-half of the AD822 being used to buffer the AD589, a 1.235 V low power reference. The output of 4.5 V can be used to drive an ADC converter front end. The other half of the AD822 is configured as a unity gain inverter and generates the other bridge input of -4.5 V . Resistor R1 and Resistor R2 provide a constant current for bridge excitation. The AD620 low power instrumentation amplifier is used to condition the differential output voltage of the bridge. The gain of the AD620 is programmed using an external resistor RG and determined by

$$
G=\frac{49.4 \mathrm{k} \Omega}{R_{G}}+1
$$



Figure 51. Low Dropout Bipolar Bridge Driver

## AD822

## OUTLINE DIMENSIONS



COMPLIANT TO JEDEC STANDARDS MS-001-BA
CONTROLLING DIMENSIONS ARE IN INCHES; MILLIMETER DIMENSIONS (IN PARENTHESES) ARE ROUNDED-OFF INCH EQUIVALENTS FOR (IN PARENTHESES) ARE ROUNDED-OFF INCRIEQUIVALENTS FOR REFERENCE ONLY AND ARE NOT APPROPRIATE FOR USE IN DESIGN.
CORNER LEADS MAY BE CONFIGURED AS WHOLE OR HALF LEADS.

Figure 52. 8-Lead Plastic Dual In-Line Package [PDIP] Narrow Body
( $\mathrm{N}-8$ )
Dimensions shown in inches and (millimeters)


## ORDERING GUIDE

| Model | Temperature Range | Package Description | Package Option | Branding |
| :--- | :--- | :--- | :--- | :--- |
| AD822AN | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 -Lead PDIP | N-8 |  |
| AD822ANZ ${ }^{1}$ | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 -Lead PDIP | N-8 |  |
| AD822AR | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 -Lead SOIC | R-8 | R-8 |
| AD822AR-REEL | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 -Lead SOIC | R-8 |  |
| AD822AR-REEL7 | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 -Lead SOIC | R-8 |  |
| AD822ARZ ${ }^{1}$ | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 -Lead SOIC | R-8 |  |
| AD822ARZ-REEL ${ }^{1}$ | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 -Lead SOIC | R-8 |  |
| AD822ARZ-REEL7 ${ }^{1}$ | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 -Lead SOIC | RM-8 | B4A |
| AD822ARM-R2 | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 -Lead MSOP | RM-8 | B4A |
| AD822ARM-REEL | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 -Lead MSOP | RM-8 | \#B4A |
| AD822ARMZ-R2 ${ }^{1}$ | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 -Lead MSOP | RM-8 |  |
| AD822ARMZ-REEL ${ }^{1}$ | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 -Lead MSOP | R-8 |  |
| AD822BR | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 -Lead SOIC | R-8 |  |
| AD822BR-REEL | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 -Lead SOIC | R-8 |  |
| AD822BR-REEL7 | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 -Lead SOIC | R-8 |  |
| AD822BRZ ${ }^{1}$ | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 -Lead SOIC | R-8 |  |
| AD822BRZ-REEL ${ }^{1}$ | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 -Lead SOIC | 8 -Lead SOIC |  |
| AD822BRZ-REEL7 ${ }^{1}$ | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 |  |  |

${ }^{1} \mathrm{Z}=\mathrm{Pb}$-free part, \# denotes lead-free product may be top or bottom marked.
SPICE model is available at www.analog.com.

## AD822

## NOTES


[^0]:    ${ }^{1} 8$-lead PDIP package: $\theta_{\mathrm{JA}}=90^{\circ} \mathrm{C} / \Omega$.
    8 -lead SOIC package: $\theta_{\mathrm{JA}}=160^{\circ} \mathrm{C} / \Omega$.
    8 -lead MSOP package: $\theta_{\mathrm{JA}}=190^{\circ} \mathrm{C} / \Omega$.

